



## Protection of Steel Using Aluminum Sacrificial Anodes in Artificial Seawater

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# PROTECTION OF STEEL USING ALUMINUM SACRIFICIAL ANODES IN ARTIFICIAL SEAWATER

Tai-Ming Tsai\*

Keywords: sacrificial anode, cathodic protection, corrosion.

## ABSTRACT

The performance of aluminum alloys used as sacrificial anodes for cathodic protection in seawater was investigated in this study. Results show that Al-3.5%Zn-0.05%In sacrificial anode alloy C has the best current efficiency, most negative open circuit potential and energy characteristics among five different Al-Zn-In alloys. Polarization curve of alloy C also shows no passivation behavior in artificial seawater. The corrosion rate of mild steel in artificial seawater was determined as a function of applied cathodic potential. The cathodic protection potential determined for mild steel in seawater was -0.78 V,SCE for a corrosion rate of less than 1 mpy. The protective area ratio of steel to sacrificial anode has been measured. Steel can be protected under the area ratio up to 4000-5000.

## INTRODUCTION

The corrosion protection of marine equipments and offshore structures can be provided by sacrificial anodes or an impressed current cathodic protection system. The protection by sacrificial anodes, although it costs generally more than that by means of an external current source, is preferred for offshore use due to its simplicity, stability and less maintenance [1,2].

Commercial anodes are either aluminum or zinc alloys for marine applications. Aluminum anodes have reliable long-term performance, and also has better current and weight characteristics than zinc anode. Aluminum anodes can be improved the performance by controlling alloy composition. Al-Zn-In, Al-Zn-Mg and Al-Zn-Sn alloys are commonly used as sacrificial anodes in marine environments [3-6].

This paper is only concerned with the behaviour

of several Al-Zn-In alloys used as anodes for cathodic protection in seawater. The effective cathodic protection potentials and protective area ratio of steel to sacrificial anode were also determined.

## EXPERIMENTAL PROCEDURE

### Performance Measurement

Cylindrical anodes 10cm high and 2cm in diameter with nominal compositions are listed in Table 1. All these cylindrical specimens were cast in steel mold, machined and polished with 600 grit emery paper, washed in acetone and quickly cleaned in a mixture of 2% chromic acid and 5% phosphoric acid at 80°C.

The performance tests for aluminum anodes were conducted by the standard method of the Japan Society of Corrosion Engineering [7]. Test specimens were covered with anti-acid tape except an exposed area of 20 cm<sup>2</sup>. The stainless steel cathode with an exposed area of 300 cm<sup>2</sup> was immersed in the one liter test cell. ASTM D 1141-75 artificial seawater was used to evaluate the performance of aluminum anodes in terms of open circuit potential (V,SCE), current capacity (Ah/kg) and current efficiency (%). A Nichia Model G1001E galvanostat was used, and the current density was maintained at 1 mA/cm<sup>2</sup> at 25±1°C for 240 hours. After test, the corroded specimens were removed and chemically cleaned in a mixture at 2% chromic acid and 5%

Table 1. Nominal Chemical Compositions of Aluminum Alloy Anodes (wt%)

Designation	Zn	In	Si	Fe	Al
Alloy A	3.5	0.01	0.04	0.05	Balance
Alloy B	3.5	0.03	0.04	0.05	Balance
Alloy C	3.5	0.05	0.04	0.05	Balance
Alloy D	2.0	0.03	0.04	0.05	Balance
Alloy E	5.0	0.03	0.04	0.05	Balance

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phosphoric acid at 80°C, and followed by rinsing in distilled water. Each individual specimen was weighed, and the current capacity and current efficiency were calculated [6]. The open circuit potentials of aluminum anodes were measured with respect to a saturated calomel electrode (SCE).

#### Galvanic Coupling Measurement

Cathodic protection is widely used to prevent or reduce the corrosion rate of marine structures. The aluminum alloy sacrificially corrodes to protect the steel structures, while it cathodically polarizes the steel to a potential below that of steel's open circuit potential. An applied potential must be adequate, otherwise the steel will be corroded or overprotected. In some cases, the large cathodic overvoltage will impair the mechanical properties [8] of the steel. The potential of steel specimen (3 cm × 3 cm) was maintained at the chosen value with a Nichia model G1001E potentiostat in artificial seawater at 25±1°C for 240 hours. After test, the steel specimen was removed and chemical cleaned in a mixture of 1 g/l hexamethylenetetramine and 10% chloric acid, and followed by rinsing distilled water. Each individual specimen was weighed, and the corrosion rates of mild steel at various cathodic potentials can be calculated.

The materials chosen for galvanic couple experiments were alloy C and mild steel. The nominal compositions of the steel are 0.05% C, 0.21% Si, 0.23% Mn, 0.01% P, and 0.01% S. Alloy C were cast, cut into flat coupons and contacted with a steel plate. The surface area of Alloy C contact with the test solution was varied from 0.30 to 38.8 cm<sup>2</sup>. One side and all edges of steel cathode were also covered with anti-acid tape, the exposed area of steel is 34 cm × 41 cm. The area ratios of the steel to Alloy C were varied from 36:1 to 4647:1, and the equipotential plot on steel was measured with a potentiostat.

Specimens for polarization tests were initially stabilized for 1 hour, and the polarization curves were determined at a scan rate of 0.1 mv s<sup>-1</sup>.

## RESULTS AND DISCUSSION

#### Performance Measurement

The variations of open circuit potentials, current capacities and current efficiencies for five different aluminum anodes are listed in Table 2. The stabilized open circuit potentials are in the range of -1.07 ~ -1.13 V, SCE. The current capacity was calculated by dividing total accumulated current

Table 2. Results of Performance Test

Designation	Open Circuit Potential (V,SCE)	Current Capacity (Ah/kg)	Current Efficiency (%)
Alloy A	-1.07	2590	88
Alloy B	-1.11	2620	89
Alloy C	-1.13	2680	91
Alloy D	-1.11	2680	91
Alloy E	-1.10	2600	89

output by weight loss of the anode. The performance of aluminum anodes is strongly influenced by the addition of alloying elements. Results show that Al-3.5%Zn-0.05%In sacrificial anode (alloy C) has the best current capacity (2680 Ah/kg), current efficiency (91%) and most negative open circuit potential (-1.13 V,SCE) among five tested alloys. Even small amount of indium in Al-Zn-In alloy is beneficial. The microstructure of alloy C is shown in Figure 1.

#### Galvanic Coupling Measurement

To ensure that the steel specimen can be protected, a series of tests were conducted at various potentials for 240 hours. The influence of applied cathodic potential on the corrosion rate of mild steel is shown in Figure 2. The error bars illustrate the variability of the data. It is clear from the figure that a corrosion rate of less than 1 mpy can be achieved with an applied potential of -0.78 V,SCE. As the cathodic potential was increased, the corrosion rate decreased further, essentially reaching nil (undetectable weight loss) at -1.1 V,SCE. The measured effective cathodic protection (e.g., less than 1 mpy) can be achieved at potentials quite

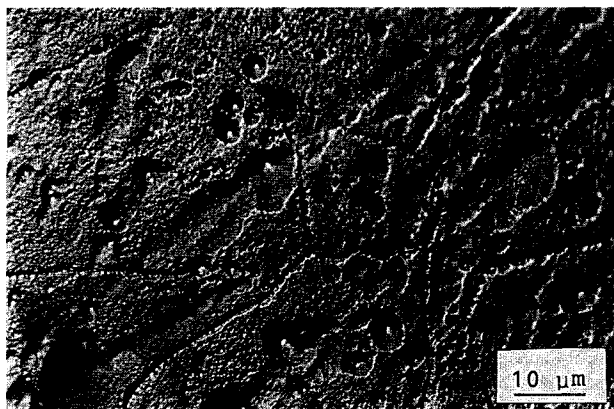


Fig. 1. Optical micrograph of alloy C.

close to the  $-0.850$  V, Cu-CuSO<sub>4</sub> reference electrode criterion [9]. It is also clear from Figure 2 that effective cathodic protection would be afforded to steel from a sacrificial anode capable of maintaining a coupled potential of  $\sim -0.78$  V,SCE. A corrosion rate under cathodic protection of 0.01 mpy or less

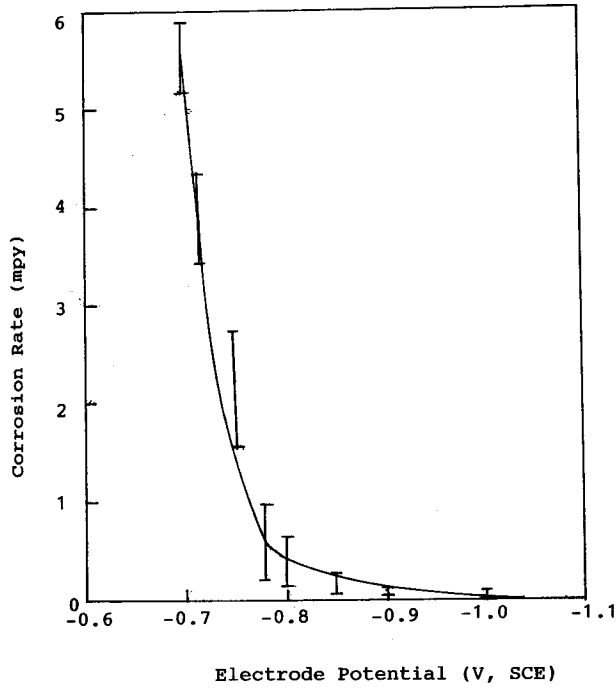


Fig. 2. Corrosion rate of mild steel in artificial seawater at 25°C as a function of cathodic potential.

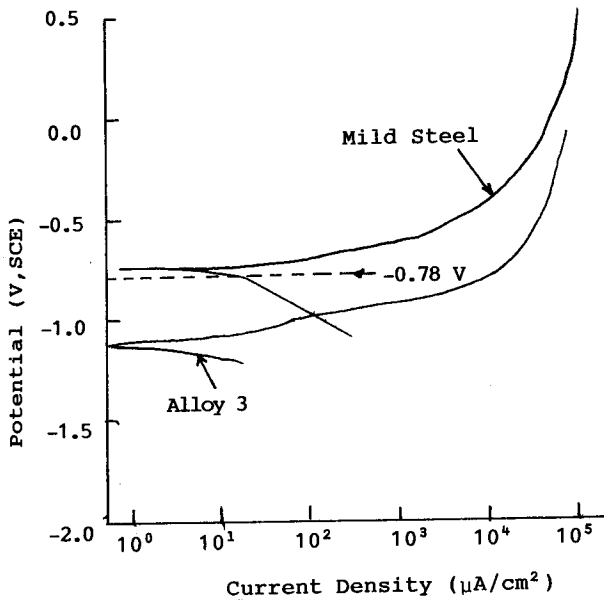


Fig. 3. Polarization curves for steel and alloy C in artificial seawater.

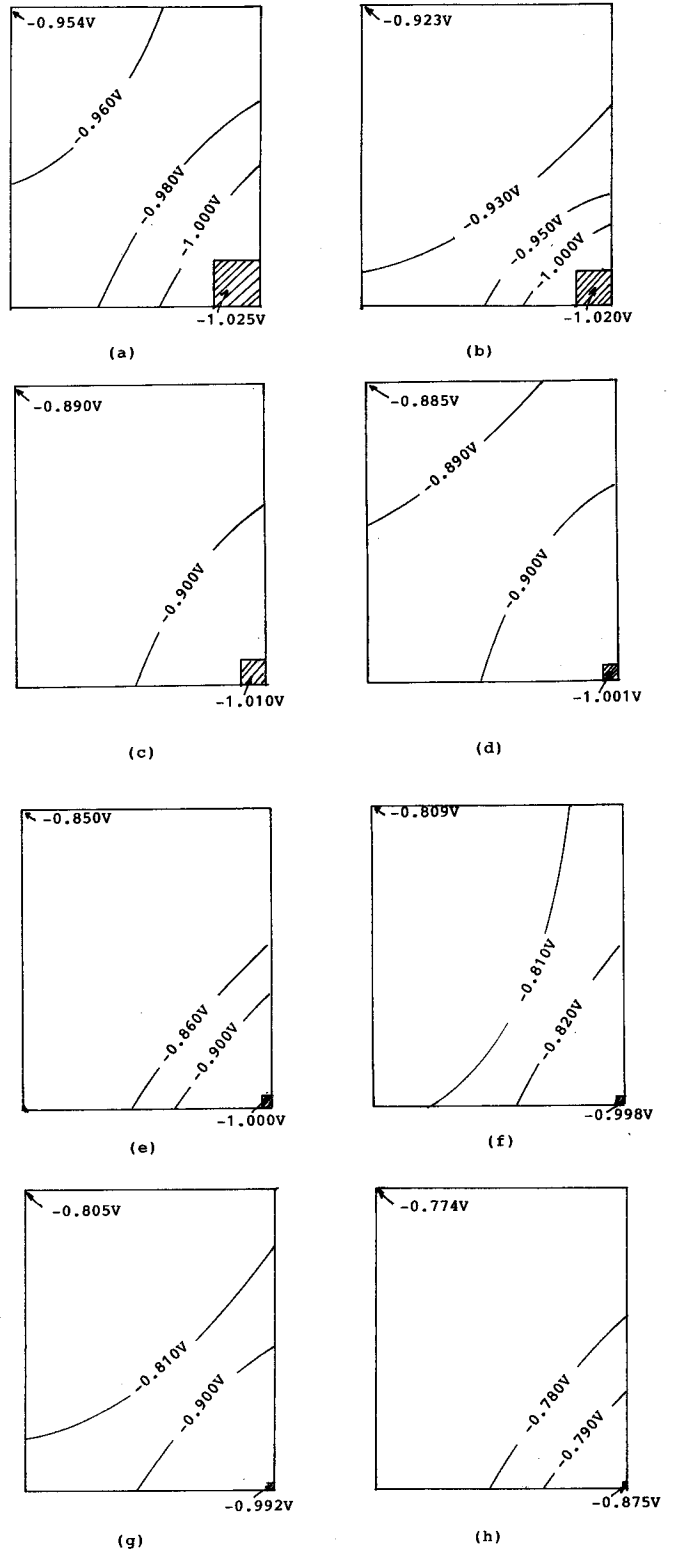


Fig. 4. Equipotential distribution on steel, exposed area of steel is 34 cm × 41 cm and exposed area of alloy C are (a) 38.8 (b) 19.4 (c) 9.7 (d) 4.85 (e) 2.43 (f) 1.21 (g) 0.61 (h) 0.30 cm<sup>2</sup> respectively.

is admirable but may be wasteful as well [10]. The more active (negative) metal in a galvanic couple is anodically oxidized. Figure 3 shows the polarization curves of mild steel and alloy C in artificial seawater. No passive region was observed for alloy C. Thus, mild steel can be cathodically protected by installation of a sacrificial anode. Criteria for cathodic protection to a potential where Tafel behaviour achieved are also recommended by the National Association of Corrosion Engineering [9]. In this study, the measured effective cathodic potential at  $-0.78$  V,SCE, is just located within the cathodic Tafel region in Figure 3.

Using the above measured value of cathodic potential as a criterion for protection, a systematic study at the protecting area ratio of steel to sacrificial anode was conducted in artificial seawater. Flat specimens of steel were electrically contacted to various size of alloy C to determine the protective area ratio of steel to alloy C. The area ratio of steel to alloy C is varied from 36:1 to 4647:1. The coupled potential contours on steel were determined and shown in Figure 4(a)-(h). alloy C is coupled on the corner of steel specimen. The coupled potential on the alloy C shows much more negative than that on the opposite corner. The least negative coupled potential on the steel at various area ratios of steel to alloy C is shown in Figure 5. It is clear from Figure 5 that a protective area ratio can be up to 4000-5000 with a coupled potential of  $-0.78$  V,SCE.

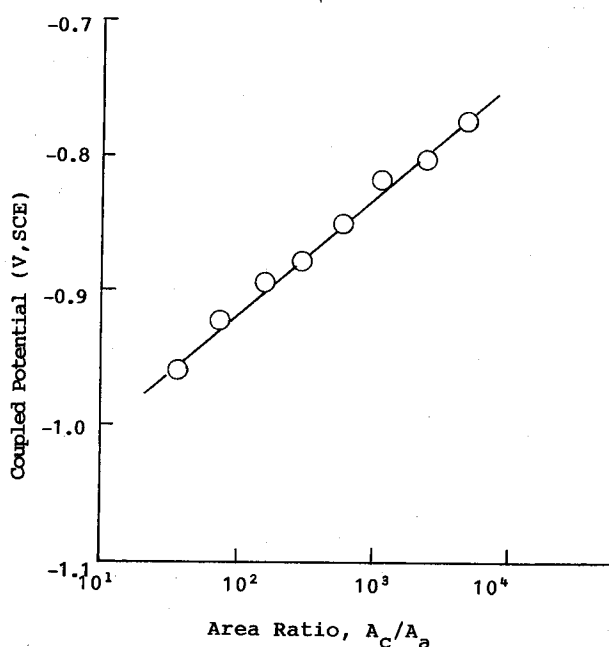


Fig. 5. The least negative coupled potential on steel as a function of steel to alloy C area ratio in artificial seawater at 25 °C.

## CONCLUSIONS

On the basis of the data presented, the following conclusions can be drawn:

1. The performance of aluminum anodes is strongly influenced by the type and concentration of the alloying elements. Even small amount of In (0.05%) in Al-Zn-In alloy is very beneficial.
2. The effective cathodic protection potential determined for mild steel in artificial seawater was  $-0.78$  V,SCE.
3. The above critical cathodic protection potential can be used as a criterion to design the protective area of steel structures.

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## REFERENCES

1. J.D. Gleason, *Materials Performance*, 17, 9 (1978).
2. R.L. Kean, L. Woolf and M.E. Beardsley, *Metals and Materials*, 6, 792 (1990).
3. R.H. Heidersbach, R. Baxter, J.S. Smart and M. Haroun; *The Metal Handbook*, 9th. Edition, Vol. 13, (Metals Park, OH; ASM, 1988), p. 921.
4. J.B. Bessone, R.A. Suarez Baldo and S.M. De De Micheli; *Corrosion*, 37, p. 533 (1981).
5. J.C. Lin and H.C. Shih; *J. Electrochem. Soc.*, 134, p. 817 (1987).
6. T. Kobayashi and Y. Tamura, "Performance of New Aluminum Alloy Anodes in Sea Water Environments," *4th. Asian-Pacific Corrosion Control Conference*, Vol. 1, p. 1, in Tokyo, Japan (1985).
7. Japan Society of Corrosion Engineering, *Boshoku Gijutsu*, 31, p. 612 (1982).
8. A. Oni and J.T. Ashaolu, *Corrosion Prevention and Control*, 38, p. 20 (1991).
9. Control of External Corrosion on Underground or Submerged Metallic Piping Systems, NACE Standard Rp-01-69, NACE, Houston (1983).
10. D.A. Jones, *Principles and Prevention of Corrosion*, Macmillan Publishing Company, New York, p. 437.

## 海洋環境中使用鋁犧牲陽極保護鋼材之研究

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### 摘要

本研究討論鋁、鋅合金製作的犧牲陽極用於陰極保護的性狀；結果顯示：合金C(Al-3.5%Zn-0.05%In)之犧牲陽極，在五種Al-Zn-In合金中有最佳的電流效率、最大的電流容量與最負之開路電位，極化曲線圖中顯示：合金C在人工海水中亦無鈍化行為發生。軟鋼在人工海水之腐蝕速率可由所施加之陰極電位決定，亦即兩者呈一簡單函數；由圖2知，陰極保護電位在-0.78 V,SCE時，軟鋼在海水之腐蝕速率低於1 mpy。保護面積比量測結果顯示，鋼材與陽極面積比大至4000-5000時仍可被鋁陽極保護。