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# AN EFFECTIVE METHOD IN BEM FOR POTENTIAL PROBLEMS OF THIN BODIES

Yao-Ming Zhang\* and Yan Gu\*

Key words: potential problem, thin body problem, BEM, nearly singular integrals.

## ABSTRACT

The study of the effective methods dealing with problems with thin domains is an important and a difficult issue in boundary element method (BEM). For the special structures of thin bodies, the singular and nearly singular integrals often occur simultaneously in boundary integral equations (BIEs). Therefore, the conventional boundary element method (CBEM) is invalid to obtain accurate results. This paper based on the indirect variable regularized BIEs of plane potential problems, and a nonlinear variable transformation is introduced in order to improve the rapid variations of nearly singular integrals. By doing these, the boundary singular and nearly singular integrals can all be evaluated effectively. Numerical examples demonstrate that the present method can deal with thin-body problems with the thickness-to-length ratios range from  $1.0E-01$  to  $1.0E-10$ .

## I. INTRODUCTION

Thin bodies, as a special structure, are frequently used for the design in various industrial applications, such as surface coated structures, thin shell-like structures, and cracks. However, the analysis of the behavior of these structures represents a very challenging and attractive task to scientists and engineers due to their special structures.

The BEM as an important numerical method has been widely used in many areas, but the accuracy of its calculation depends heavily on the computational precision of the singular and nearly singular integrals [1-4, 6, 7, 10, 11, 18, 22, 23]. For non-thin body structures, there are two issues of major concern in BEM-based simulation. One is the estimation of singular integrals when the source point and the field point coincide; the other is known as the boundary layer effect when the physical quantities at the interior points very close to the boundary are calculated. However, for thin body structures,

some boundary elements will be very close to each other. Thus, the singular and nearly singular integrals need to be evaluated simultaneously when calculating the boundary unknown variables. Furthermore, almost all the field points are very close to the boundary and cannot be obtained accurately by Gauss quadrature. Consequently, the BEM analyses of thin body problems require not only the regularization BIEs to evaluate the singular integrals, but also an effective algorithm to calculate the nearly singular integrals.

Many technologies and methods of evaluating nearly singular integrals have been developed in recent years. Those methods can be divided on the whole into two categories: "indirect algorithms" and "direct algorithms". The indirect algorithms are mainly to calculate indirectly or avoid calculating the nearly singular integrals by establishing new regularized BIEs, such as virtual boundary element method [21, 27], rigid-body displacement method or the simple solution method [13], as well as other methods [5, 16, 19]. The direct algorithms are calculating the nearly singular integrals directly. They mainly include interval subdivision method [9], special Gaussian quadrature method [14], transformations methods [8, 15, 26], and exact integration methods [17, 24, 28]. These methods obtained varying degree of success, but the questions still remain [26]. At the same time, the analysis of thin-body problems by BEM has also been sequentially carried out. Sladek *et al.* have obtained amount of the original results in this field. Non-singular integral equations for thin-walled structures are proposed based on a subtraction technique and mathematical regularization [20]. Liu *et al.* have undertaken a lot of researches [12] based on the non-linear coordinate transformation. Zhou *et al.* proposed semi-analytical and analytical integral algorithms to deal with thin-body problems [29, 30]. It's necessary to point out that almost all the existing methods are based on the direct formulation. Thus the super-singular and nearly super-singular integrals should be dealt with in the solving process.

In this paper, the regularized BIEs [25] are combined with the nonlinear variable transformation [26] to analyze thin body problems. Owing to the special geometric shape of thin body structures, this combination is extraordinary. By doing these, the singular integrals can be estimated accurately by using the regularized BIEs, and the rapid variations of the nearly singular kernels can be smoothed out effectively by using the

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proposed nonlinear transformation. Then the singular and nearly singular integrals can all be evaluated accurately with conventional Gaussian quadrature. Two examples on heat conduction in thin domains with thickness-to-length ratios range from 1E-01 to 1E-09 are presented to test the proposed method. Both boundary unknown variables on the boundary and physical quantities at interior points are calculated, from which we can see that the suggested method is effective and feasible to deal with thin body problems.

## II. THE EQUIVALENT NONSINGULAR BOUNDARY INTEGRAL EQUATIONS

In this paper, we always assume that  $\Omega$  is a bounded domain in  $R^2$ ,  $\Omega^c$  its open complement domain, and  $\Gamma = \partial\Omega$  their common boundary. In BEM, if boundary conditions are given properly, the domain variables can be computed by corresponding integral equations after the boundary quantities are all obtained. The equivalent non-singular BIEs with indirect variables are given in [25]. For the domain  $\Omega$ , the BIEs are given as

$$\int_{\Gamma} \phi(\mathbf{x}) d\Gamma_x + \int_{\Omega} f(\mathbf{x}) d\Omega = 0 \quad (1)$$

$$u(\mathbf{y}) = \int_{\Gamma} \phi(\mathbf{x}) u^*(\mathbf{x}, \mathbf{y}) d\Gamma_x + \int_{\Omega} f(\mathbf{x}) u^*(\mathbf{x}, \mathbf{y}) d\Omega + C, \mathbf{y} \in \Gamma \quad (2)$$

$$\begin{aligned} \nabla u(\mathbf{y}) &= \phi(\mathbf{y}) + \int_{\Gamma} [\phi(\mathbf{x}) - \phi(\mathbf{y})] \nabla u^*(\mathbf{x}, \mathbf{y}) d\Gamma \\ &- \phi(\mathbf{y}) \left\{ \int_{\Gamma} [\mathbf{t}(\mathbf{x}) - \mathbf{t}(\mathbf{y})] \frac{\partial u^*(\mathbf{x}, \mathbf{y})}{\partial \mathbf{t}_x} d\Gamma \right. \\ &+ \left. \int_{\Gamma} [\mathbf{n}(\mathbf{x}) - \mathbf{n}(\mathbf{y})] \frac{\partial u^*(\mathbf{x}, \mathbf{y})}{\partial \mathbf{n}_x} d\Gamma \right\} \\ &+ \int_{\Omega} f(\mathbf{x}) \nabla u^*(\mathbf{x}, \mathbf{y}) d\Omega \end{aligned} \quad (3)$$

where  $\mathbf{t}(\mathbf{x})$ ,  $\mathbf{n}(\mathbf{x})$  are the unit tangent and outward normal vectors of  $\Gamma$  to domain  $\Omega$  at point  $\mathbf{x}$  respectively.

For the domain  $\Omega^c$ , the equations are given as

$$\int_{\Gamma} \phi(\mathbf{x}) d\Gamma_x + \int_{\Omega^c} f(\mathbf{x}) d\Omega^c = 0 \quad (4)$$

$$u(\mathbf{y}) = \int_{\Gamma} \phi(\mathbf{x}) u^*(\mathbf{x}, \mathbf{y}) d\Gamma_x + \int_{\Omega^c} f(\mathbf{x}) u^*(\mathbf{x}, \mathbf{y}) d\Omega^c + C, \mathbf{y} \in \Gamma \quad (5)$$

$$\begin{aligned} \nabla_y u(\mathbf{y}) &= \int_{\Gamma} [\phi(\mathbf{x}) - \phi(\mathbf{y})] \nabla_y u^*(\mathbf{x}, \mathbf{y}) d\Gamma_x \\ &- \phi(\mathbf{y}) \left\{ \int_{\Gamma} [\mathbf{t}^c(\mathbf{x}) - \mathbf{t}^c(\mathbf{y})] \nabla_y u^*(\mathbf{x}, \mathbf{y}) \cdot \mathbf{t}^c(\mathbf{x}) d\Gamma_x \right. \\ &+ \left. \int_{\Gamma} [\mathbf{n}^c(\mathbf{x}) - \mathbf{n}^c(\mathbf{y})] \nabla_y u^*(\mathbf{x}, \mathbf{y}) \cdot \mathbf{n}^c(\mathbf{x}) d\Gamma_x \right\} \\ &+ \int_{\Omega^c} f(\mathbf{x}) \nabla_y u^*(\mathbf{x}, \mathbf{y}) d\Omega^c \end{aligned} \quad (6)$$

where  $\mathbf{t}^c(\mathbf{x})$ ,  $\mathbf{n}^c(\mathbf{x})$  are the unit tangent and outward normal vectors of  $\Gamma$  to domain  $\Omega^c$  at point  $\mathbf{x}$  respectively.

For the interior point  $\mathbf{y}$ , the integral equations can be written as

$$u(\mathbf{y}) = \int_{\Gamma} \phi(\mathbf{x}) u^*(\mathbf{x}, \mathbf{y}) d\Gamma + \int_{\hat{\Omega}} f(\mathbf{x}) u^*(\mathbf{x}, \mathbf{y}) d\hat{\Omega} + C, \mathbf{y} \in \hat{\Omega} \quad (7)$$

$$\begin{aligned} \nabla u(\mathbf{y}) &= \int_{\Gamma} \phi(\mathbf{x}) \nabla_y u^*(\mathbf{x}, \mathbf{y}) d\Gamma \\ &+ \int_{\hat{\Omega}} f(\mathbf{x}) \nabla_y u^*(\mathbf{x}, \mathbf{y}) d\hat{\Omega}, \mathbf{y} \in \hat{\Omega} \end{aligned} \quad (8)$$

In (1)-(8),  $\phi(\mathbf{x})$  is the density function to be determined,  $f(\mathbf{x})$  the body function, and in (7) and (8)  $\hat{\Omega} = \Omega$  or  $\Omega^c$ .

The density function  $\phi(\mathbf{x})$  and boundary quantities can be obtained via (1)-(3) or (4)-(6). However, if the domain of the problem is thin, the distance  $r$  between some boundary nodes and integral elements probably approaches zero. This would cause nearly singular integrals in (2)-(3) and (5)-(6), and the boundary unknowns cannot be calculated accurately by Gauss quadrature. On the other hand, the field points are usually very close to the integral elements for thin-body problems. Therefore, there also exist nearly singular integrals in (7)-(8). These integrals can be expressed as

$$I_1 = \int_{\Gamma} \phi(\mathbf{x}) \ln r^2 d\Gamma, I_2 = \int_{\Gamma} \phi(\mathbf{x}) \frac{1}{r^{2\alpha}} d\Gamma \quad (9)$$

where  $\alpha > 0$  and  $\phi(\mathbf{x})$  is a well-behaved function. Obviously, the nearly singularities of the integrals in (9) come from the distance  $r$ .

## III. THE TRANSFORMATION OF NEARLY SINGULAR INTEGRAL

### 1. Linear Element Approximation of the Boundary $\Gamma$

Assuming  $\mathbf{x}^1 = (x_1^1, x_2^1)$ ,  $\mathbf{x}^2 = (x_1^2, x_2^2)$  are the two extreme points of the linear element  $\Gamma_j$ , then the element  $\Gamma_j$  can be expressed as

$$x_k(\xi) = N_1(\xi) x_k^1 + N_2(\xi) x_k^2, \xi \in [-1, 1], k = 1, 2 \quad (10)$$

here  $N_1(\xi) = (1 - \xi)/2$ ,  $N_2(\xi) = (1 + \xi)/2$ . Letting  $s_i = x_i^2 - x_i^1$ ,  $w_i = y_i - (x_i^2 + x_i^1)/2$ , one has

$$r_i = \frac{r_i}{r} = \frac{y_i - x_i}{r} = \frac{s_i \xi / 2 + w_i}{r} \quad (11)$$

$$\begin{aligned} r^2 &= |\mathbf{x} - \mathbf{y}|^2 = r_i r_i = A\xi^2 + B\xi + E \\ &= L^2[(\xi - \eta)^2 + d^2] \end{aligned} \quad (12)$$

where  $A = s_i s_i / 4$ ,  $B = s_i w_i$ ,  $E = w_i w_i$ ,  $\eta = -B / 2A$ ,  $L = \sqrt{A}$ ,  $d = \sqrt{4AE - B^2} / 2A$ .

The integrals  $I_1$  and  $I_2$  in (9) can be divided into two parts at point  $\eta$  as follows

$$\begin{aligned} I_1 &= \left\{ \int_{-1}^{\eta} + \int_{\eta}^1 \right\} g(\xi) \ln[(\xi - \eta)^2 + d^2] d\xi \\ &\quad + \ln L^2 \int_{-1}^1 g(\xi) d\xi \end{aligned} \quad (13)$$

$$I_2 = \left\{ \int_{-1}^{\eta} + \int_{\eta}^1 \right\} \frac{g(\xi)}{L^{2\alpha} [(\xi - \eta)^2 + d^2]^\alpha} d\xi \quad (14)$$

where  $g(\cdot)$  is a regular function that consists of shape function and Jacobian.

## 2. ‘‘Arc Element’’ Approximation of the Boundary $\Gamma$

In engineering applications, the structures with circle or ellipse boundaries are widely used in order to avoid stress concentration. Suppose  $(R, \theta_1)$ ,  $(R, \theta_2)$  are the coordinates of the two extreme points of the arc element  $\Gamma_j$  respectively. Then the element  $\Gamma_j$  can be expressed as [25]

$$\begin{cases} x_1 = R \cos \theta \\ x_2 = R \sin \theta \end{cases}, \theta = \frac{1 - \xi}{2} \theta_1 + \frac{1 + \xi}{2} \theta_2, \xi \in [-1, 1]$$

For the interior point  $\mathbf{y} = (R_0 \cos \theta_0, R_0 \sin \theta_0)$ ,  $\theta_1 < \theta_0 < \theta_2$ . Then  $\theta_0 = \frac{1 - \eta}{2} \theta_1 + \frac{1 + \eta}{2} \theta_2$ , thus

$$r^2 = |\mathbf{x} - \mathbf{y}|^2 = 4RR_0 \{ \sin^2 [\beta(\xi - \eta)] + d^2 \} \quad (15)$$

here  $\gamma = \beta(\xi - \eta)$ ,  $\beta = \frac{\theta_2 - \theta_1}{4}$ ,  $d = \frac{R - R_0}{4\sqrt{RR_0}}$ .

The integrals  $I_1$  and  $I_2$  in (9) can be divided into two parts at point  $\eta$  as follows

$$\begin{aligned} I_1 &= \left\{ \int_{-1}^{\eta} + \int_{\eta}^1 \right\} g(\xi) \ln(\sin^2 \gamma + d^2) d\xi \\ &\quad + \ln L^2 \int_{-1}^1 g(\xi) d\xi \end{aligned} \quad (16)$$

$$I_2 = \frac{1}{L^{2\alpha}} \left\{ \int_{-1}^{\eta} + \int_{\eta}^1 \right\} \frac{g(\xi)}{(\sin^2 \gamma + d^2)^\alpha} d\xi \quad (17)$$

where  $L = 2\sqrt{RR_0}$  and  $g(\cdot)$  is the regular function that consists of shape function and Jacobian.

## 3. The Transformation

The integrals  $I_1$  and  $I_2$  in (13), (14), (16), and (17) can be reduced to the following integrals by simple deduction

$$\begin{aligned} T_1 &= \int_0^A g(x) \ln(x^2 + d^2) dx, \\ T_2 &= \int_0^A \frac{g(x)}{(x^2 + d^2)^\alpha} dx \end{aligned} \quad (18)$$

Adopting the following variable transformation

$$x = d(e^{k(1+t)} - 1), t \in [-1, 1], k = \ln \sqrt{1 + A/d}$$

Equation (18) can be rewritten as

$$\begin{aligned} T_1 &= dk \int_{-1}^1 g(t) \ln d^2 e^{k(1+t)} dt \\ &\quad + dk \int_{-1}^1 g(t) \ln[(e^{k(1+t)} - 1)^2 + 1] e^{k(1+t)} dt \\ T_2 &= d^{1-2\alpha} k \int_{-1}^1 \frac{g(t) e^{k(1+t)}}{[e^{k(1+t)} - 1]^2 + 1]^\alpha} dt \end{aligned} \quad (19)$$

The final integral formulations are obtained as shown in (19), which can now be calculated accurately by standard Gaussian quadrature.

## IV. NUMERICAL EXAMPLES

Two examples on heat conduction in thin domains are presented in this section to test the proposed method. Boundary unknown variables on the boundary and physical quantities at interior points are both calculated. Only the Gaussian quadrature is used to calculate the numerical integrals, including the nearly singular integrals.

**Example 1.** Heat conduction in a thin cylinder is considered. The inner and outer radii of the cylinder is  $a = 10$  and  $b$  respectively. The boundary conditions are given in Fig. 1.

Eighty arc elements are divided on the boundaries totally. Thirty-four arc elements are divided on the inner and outer cylinders, and six are on the two short straight boundaries.

Linear discontinuous interpolation is adopted to approximate the boundary functions. In this example,  $(b - a)/a$  is defined as the thickness-to-length ratio [29].

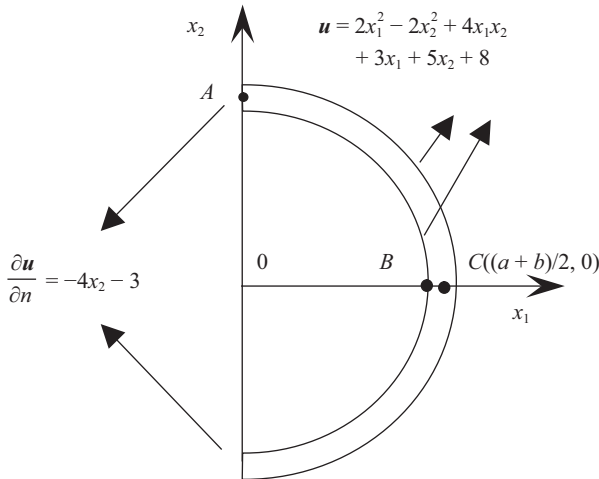
For different thickness-to-length ratio, Table 1 and Table 2 show that the potential at boundary node  $A$  can be well calculated by the present method and CBEM. However, the flux results calculated by the CBEM at the node  $B$  begin to degenerate when the thickness-to-length ratio less than 1.0E-02. In contrast, the present method can be used to calculate the

**Table 1. Temperatures at the boundary node A.**

$(b - a)/a$	Exact	CBEM	Relative error (%)	Present	Relative error (%)
1.0E-01	-0.1600000E+03	-0.1600002E+03	-0.1367549E-03	-0.1600002E+03	-0.1367549E-03
1.0E-02	-0.1437550E+03	-0.1437477E+03	0.5103898E-02	-0.1437516E+03	0.2373698E-02
1.0E-03	-0.1421750E+03	-0.1417780E+03	0.2792951E+00	-0.1421704E+03	0.3246838E-02
1.0E-04	-0.1420175E+03	-0.1413651E+03	0.4593660E+00	-0.1420128E+03	0.3339321E-02
1.0E-05	-0.1420018E+03	-0.1413419E+03	0.4646742E+00	-0.1419970E+03	0.3348576E-02
1.0E-06	-0.1420002E+03	-0.1413403E+03	0.4647293E+00	-0.1419954E+03	0.3349502E-02
1.0E-07	-0.1420000E+03	-0.1413401E+03	0.4647299E+00	-0.1419953E+03	0.3349594E-02
1.0E-08	-0.1420000E+03	-0.1413401E+03	0.4647299E+00	-0.1419952E+03	0.3349604E-02
1.0E-09	-0.1420000E+03	-0.1413401E+03	0.4647299E+00	-0.1419952E+03	0.3349605E-02
1.0E-10	-0.1420000E+03	-0.1413401E+03	0.4647299E+00	-0.1419952E+03	0.3349605E-02

**Table 2. Normal gradients at the boundary node B.**

$(b - a)/a$	Exact	CBEM	Relative error (%)	Present	Relative error (%)
1.0E-1	-0.4300000E+02	-0.4296942E+02	0.7111454E-01	-0.4296942E+02	0.7111454E-01
1.0E-2	-0.4300000E+02	-0.4297181E+02	0.6555491E-01	-0.4297172E+02	0.6576947E-01
1.0E-3	-0.4300000E+02	-0.1257396E+03	-0.1924176E+03	-0.4296923E+02	0.7155983E-01
1.0E-4	-0.4300000E+02	0.3594451E+01	0.1083592E+03	-0.4296865E+02	0.7290199E-01
1.0E-5	-0.4300000E+02	0.3649202E-01	0.1000849E+03	-0.4296859E+02	0.7305539E-01
1.0E-6	-0.4300000E+02	0.5539044E-03	0.1000013E+03	-0.4296838E+02	0.7352498E-01
1.0E-7	-0.4300000E+02	-0.1047532E-02	0.9999756E+02	-0.4296336E+02	0.8520952E-01
1.0E-8	-0.4300000E+02	-0.1734616E-02	0.9999597E+02	-0.4296412E+02	0.8345282E-01
1.0E-9	-0.4300000E+02	0.3270279E-02	0.1000076E+03	-0.4295924E+02	0.9478312E-01
1.0E-10	-0.4300000E+02	0.1252932E-01	0.1000291E+03	-0.4294596E+02	0.1256806E+00



**Fig. 1. A thin-walled ring.**

fluxes accurately even when the thickness-to-length ratio as small as 1.0E-10. The above analysis indicates that the CBEM can only be available to calculate the acceptable boundary unknown variables for the thickness-to-length ratio down to 1.0E-02. Nevertheless, the present method can obtain the accurate results even when the thickness-to-length ratio as small as 1.0E-10.

Table 3 gives the results of fluxes at interior point C for

different thickness-to-length ratio, from which it can be seen that the CBEM begin to degenerate when the thickness-to-length ratio down to 1.0E-02, with further decrease of the thickness-to-length ratio, the results are out of true. However, the results obtained by using the present method are excellently consistent with the analytical solutions even when the thickness-to-length ratio equals 1.0E-09. The dates in Table 4 further demonstrate the effectiveness of the present method when the interior points gradually close to the boundary with thickness-to-length ratio equals 1.0E-09.

For different thickness-to-length ratio, the temperature errors at interior point C are shown in Fig. 2. It can be seen that the potential results obtained by using the present method are in good agreement with the exact solutions.

The convergence curves of computed fluxes at interior points B and C are shown in Fig. 3, from which we can observe that the convergence speeds are still fast even when the thickness-to-length ratio reached 1.0E-09.

**Example 2.** Heat conduction in a thin rectangle is considered. The length and width of the rectangular are  $a = 1$  and  $b$ . The boundary conditions are given in Fig. 4.

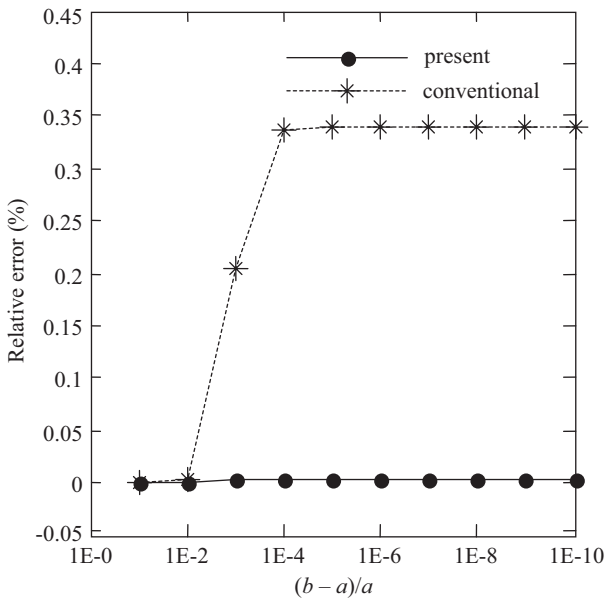
Thirty arc elements are divided on the two long sides totally, and only two elements are divided on the two short sides for their little length. Therefore, the total number of the element is

**Table 3. Fluxes  $\partial u/\partial x_1$  at the interior node C.**

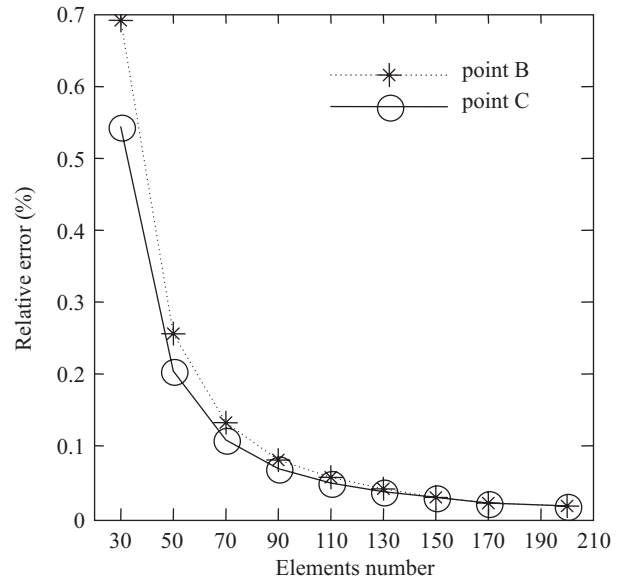
$(b - a)/a$	Exact	CBEM	Relative error (%)	Present	Relative error (%)
1.0E-01	0.4500000E+02	0.4499943E+02	0.1270766E-02	0.4499943E+02	0.1270766E-02
1.0E-02	0.4320000E+02	0.4268257E+02	0.1197752E+01	0.4317559E+02	0.5650029E-01
1.0E-03	0.4302000E+02	0.2008537E+02	0.5331156E+02	0.4298930E+02	0.7135087E-01
1.0E-04	0.4300200E+02	-0.1064946E+00	0.1002477E+03	0.4297069E+02	0.7281246E-01
1.0E-05	0.4300020E+02	-0.1021886E-02	0.1000024E+03	0.4296872E+02	0.7320819E-01
1.0E-06	0.4300002E+02	-0.1021467E-04	0.1000000E+03	0.4296856E+02	0.7317052E-01
1.0E-07	0.4300000E+02	-0.1021430E-06	0.1000000E+03	0.4297031E+02	0.6905575E-01
1.0E-08	0.4300000E+02	-0.1023443E-08	0.1000000E+03	0.4296983E+02	0.7016518E-01
1.0E-09	0.4300000E+02	-0.9865553E-11	0.1000000E+03	0.4296284E+02	0.8640969E-01
1.0E-10	0.4300000E+02	0.4707623E-12	0.1000000E+03	0.4295324E+02	0.1087370E+00

**Table 4. Fluxes  $\partial u/\partial x_1$  on the line  $x_2 = 0$  when  $(b - a)/a = 1.0E - 09$ .**

$x_1$	Exact	CBEM	Relative error (%)	Present	Relative error (%)
10.000000001	0.4300000E+02	0.8931400E-05	0.9999998E+02	0.4296523E+02	0.8087179E-01
10.000000002	0.4300000E+02	0.6698547E-05	0.9999998E+02	0.4296477E+02	0.8193783E-01
10.000000003	0.4300000E+02	0.4465695E-05	0.9999999E+02	0.4296423E+02	0.8317615E-01
10.000000004	0.4300000E+02	0.2232842E-05	0.9999999E+02	0.4296360E+02	0.8464009E-01
10.000000005	0.4300000E+02	-0.9865553E-11	0.1000000E+03	0.4296284E+02	0.8640969E-01
10.000000006	0.4300000E+02	-0.2232862E-05	0.1000000E+03	0.4296189E+02	0.8862007E-01
10.000000007	0.4300000E+02	-0.4465715E-05	0.1000000E+03	0.4296065E+02	0.9150921E-01
10.000000008	0.4300000E+02	-0.6698567E-05	0.1000000E+03	0.4295890E+02	0.9557602E-01
10.000000009	0.4300000E+02	-0.8931419E-05	0.1000000E+03	0.4295607E+02	0.1021645E+00



**Fig. 2. Temperature errors at interior point C.**



**Fig. 3. Convergence curves of fluxes at points B and C with  $(b - a)/a = 1.0E - 09$ .**

32. As we all know, the evaluation of fluxes would be more difficult than that of potential and, therefore, only the flux results are listed. The normal gradients on the boundary are given in Table 5. The flux results at interior points are given in Table 6 and Fig. 5. The convergence curve of fluxes at interior

point is shown in Fig. 6. In this example, we defined  $b/a$  is the thickness-to-length ratio [29].

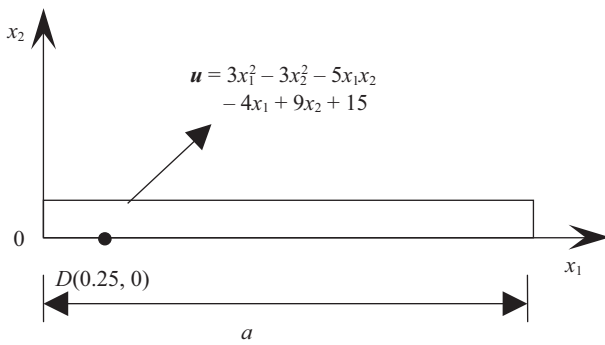
Table 5 shows that the flux results calculated by the CBEM at the boundary node  $D$  become completely invalid when the thickness-to-length ratio equals  $1.0E-03$ . In contrast with the

**Table 5. Normal gradients at the boundary node  $D$ .**

b/a	Exact	CBEM	Relative error (%)	Present	Relative error (%)
1.0E-01	-0.7750000E+01	-0.7749404E+01	0.7684617E-02	-0.7749604E+01	0.5109677E-02
1.0E-02	-0.7750000E+01	-0.7749052E+01	0.1223317E-01	-0.7749910E+01	0.1161223E-02
1.0E-03	-0.7750000E+01	-0.1067220E+02	-0.3770577E+02	-0.7749989E+01	0.1419354E-03
1.0E-04	-0.7750000E+01	0.8987383E+00	0.1115966E+03	-0.7749987E+01	0.1728589E-03
1.0E-05	-0.7750000E+01	-0.7221865E+00	0.9068146E+02	-0.7749979E+01	0.2709677E-03
1.0E-06	-0.7750000E+01	-0.8789177E+00	0.8865913E+02	-0.7749991E+01	0.1161290E-03
1.0E-07	-0.7750000E+01	-0.8945172E+00	0.8845784E+02	-0.7749973E+01	0.3467598E-03
1.0E-08	-0.7750000E+01	-0.8960764E+00	0.8843772E+02	-0.7750015E+01	-0.1949624E-03
1.0E-09	-0.7750000E+01	-0.8962323E+00	0.8843571E+02	-0.7750183E+01	-0.2361732E-02
1.0E-10	-0.7750000E+01	-0.8962479E+00	0.8843551E+02	-0.7750283E+01	-0.3656933E-02

**Table 6. Fluxes  $\partial u/\partial x_1$  at the interior points on the line  $x_1 = 0.3$  when  $b/a = 1.0E - 09$ .**

$x_2$	Exact	CBEM	Relative error (%)	Present	Relative error (%)
1.0E-10	-0.2200000E+01	-0.4007663E+01	-0.8216651E+02	-0.2201486E+01	-0.6756812E-01
2.0E-10	-0.2200000E+01	-0.4007663E+01	-0.8216651E+02	-0.2201486E+01	-0.6754774E-01
3.0E-10	-0.2200000E+01	-0.4007663E+01	-0.8216651E+02	-0.2201486E+01	-0.6753649E-01
4.0E-10	-0.2200000E+01	-0.4007663E+01	-0.8216651E+02	-0.2201486E+01	-0.6753603E-01
5.0E-10	-0.2200000E+01	-0.4007663E+01	-0.8216651E+02	-0.2201486E+01	-0.6753295E-01
6.0E-10	-0.2200000E+01	-0.4007663E+01	-0.8216651E+02	-0.2201486E+01	-0.6753090E-01
7.0E-10	-0.2200000E+01	-0.4007663E+01	-0.8216650E+02	-0.2201486E+01	-0.6753139E-01
8.0E-10	-0.2200000E+01	-0.4007663E+01	-0.8216650E+02	-0.2201486E+01	-0.6752422E-01
9.0E-10	-0.2200000E+01	-0.4007663E+01	-0.8216650E+02	-0.2201486E+01	-0.6754076E-01

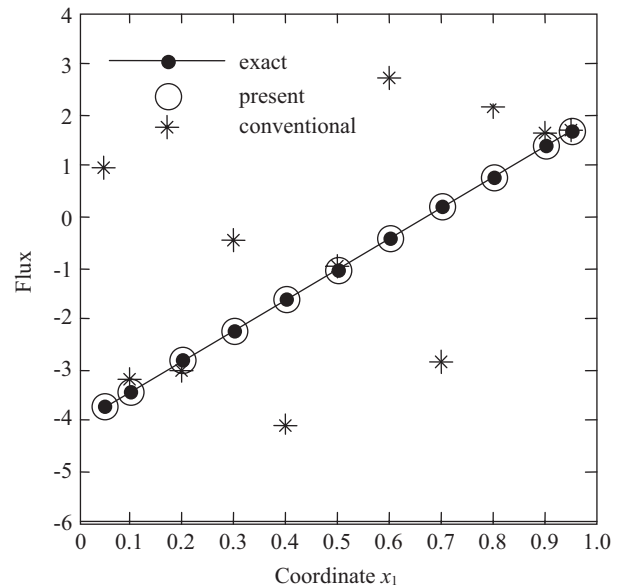


**Fig. 4. A thin rectangular domain.**

CBEM, the present method can be used to calculate the fluxes accurately even when the thickness-to-length ratio down to  $1.0E-10$ .

The flux results at interior points are shown in Table 6 and Fig. 5. It can be observed that the flux results calculated by present method represent a high degree of accuracy and stability. In addition, as shown in Fig. 6, the convergence speeds of the computed fluxes still fast even when the thickness-to-length ratio gets down to  $1.0E-09$ .

According to the above analysis, the results computed by the CBEM become less satisfactory when the thickness-to-length ratio less than  $1.0E-02$ . In contrast, the results calculated by present method are still satisfactory even when the thickness-to-length ratio as small as  $1.0E-09$ .



**Fig. 5.  $\partial u/\partial x_1$  at interior points on the line  $x_2 = 5.0E - 10$ .**

### V. CONCLUSION

In this paper, a general algorithm in BEM for potential problem of thin bodies is presented. An equivalent non-singular BIEs and a general transformation have been presented to estimate the singular and nearly singular integrals which occur in the analysis of thin body problems. With the



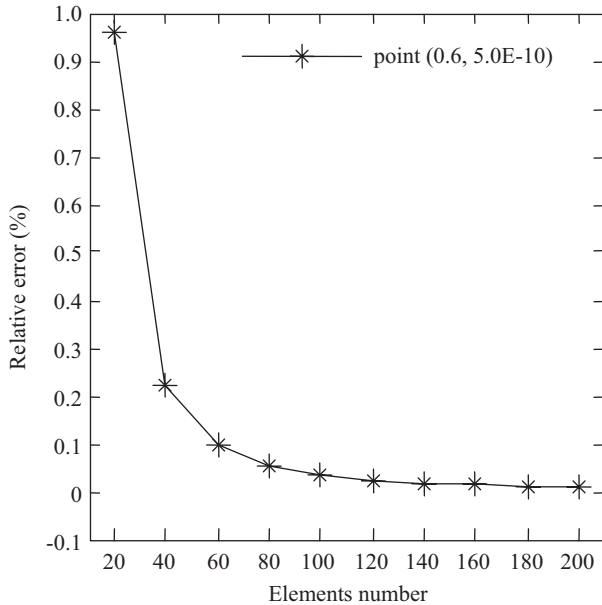


Fig. 6. Convergence curve of fluxes at points (0.6, 5.0E – 10).

proposed method, the singularities of singular and nearly singular integrals are removed efficiently, and fairly high accuracy of numerical results is achieved. Numerical examples on heat conduction in thin domains with thickness-to-length ratios range from 1E-01 to 1E-09 are presented to test the proposed method, with which excellent results are obtained. The present method is also general and can be applied to other problems in BEM, which will be discussed later.

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